# ADVANTAGE STEEL

Steel Bridges: Leveraging the performance and versatility of structural steel for building Canada's infrastructure

Rehabilitation of three expressway bridges in Toronto

Restoring Red Willow River Bridge: An orthotropic steel deck solution

Port Mann Bridge: Expanding a Vancouver centrepiece



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# ADVANTAGE STEEL

#### NO 49 SPRING 2014



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By Ed Whalen, P.Eng. President



### GCs galvanize the Canadian trade contractors

recently attended a pirate-themed construction association event in Saskatoon. As a mixed trade event, there were jokes about the thieves and pirates in the construction industry, and we all laughed in jest. It was a great evening, and somewhat of a foreshadowing event, as it turns out.

A few weeks later I witnessed what I personally call the final proof of why Canada desperately needs prompt payment legislation. The general contractors in the pirate form of the Fair Payment Reform Ontario (F-PRO) coalition showed their true colours, hoisted the pirate flag and opened the cannon doors when the *Prompt Payment Act*, or Bill 69, was quickly advanced into the Ontario Legislature Subcommittee by the Liberal government. The general contractors, as it turns out, never expected the National Trade Contractors Coalition of Canada (NTCCC) to get Bill 69 to Committee. It now appears that the general contractors never intended to support what they helped co-author.

In March, Bill 69, co-authored by the National Trade Contractors Coalition of Canada and the Ontario General Contractors Association (OGCA), made its way to the Ontario Legislature Subcommittee after all-party support in the Legislature in 2013. The bill was crafted to its final form after two years of negotiations with the OGCA and NTCCC. Senior representatives from PCL, EllisDon and Bird Construction, to name a few, were all active participants.

Leading up to the Subcommittee hearings at the last minute, the OGCA was on public record supporting the bill, only to reverse its position at the last minute, stating that, "The needs of the GCs have not been addressed." What?! Give me a break! With this kind of blatant baloney, is it any wonder why trade contractors in Canada are revolting, standing up for their rights, and speaking with one voice against the general contractors' bad behaviour?

So who is this group of "fair payment reformers?" The group is listed as Eastern Construction, ACS Infrastructure Canada, Carillion, Dragados Canada, EllisDon, PCL Construction, Bird Construction and AECON. Fair Payment Reform Ontario is asking the province and the trade contractors for fairness. Am I dreaming?! These same companies participated with OGCA and had two years to get it "fair." I suppose they had to set up a separate coalition from the OGCA to save face. Maybe OGCA has lost its support or has been used as a decoy. I say a spade is a spade no matter how you brand it. Shame on them all.

There is one group that prospers from conflict in the construction industry. Lawyers fearing that prompt payment would wreak havoc on their successful business model spun panic in the industry about lien incompatibility. Although the current Ontario lien legislation is in need of an update, linking the two was ludicrous and self-serving. Further confirmation of this was their demand that they have a seat at the new Attorney General's Committee to review the *Ontario Construction Lien Act* in conjunction with prompt payment. The lawyers see themselves as stakeholders in the construction industry, profit from it, and want an equal voice at the table. Unbelievable! Everyone wants our money.

I have a suggestion that can save a whole lot of committee time, lawyers' bills, and money lost to pirates. Prompt payment should say this: "Payment shall be paid by the owner directly to the trades and within 30 days." It is evident that the general contractors are clearly entrenched in the practice of non-payment for their own profit. They have been able to get away with it for so long and believe it is their right. We must take their hand out of the cookie jar for the good of the industry and economy. As a group, they can no longer be trusted.

In a recent decision of the NTCCC, provincial chapters of the organization will be formed. This will further galvanize and strengthen the voice of the true builders of Canada. Trade contractors do all the work, employ all the people, and take all the financial risk. The trade contractors are the real leaders in the construction industry, and the NTCCC will be our collective voice.

#### **ADVANTAGE STEEL**

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CISC is not responsible for the opinions expressed in this publication by those contributing articles. Visit us at www.cisc-icca.ca or Tel 905-946-0864, Fox 905-946-8574 CHAIRMAN Jim McLagan, Canron Western Constructors Ltd. MANAGING EDITOR Tareq Ali, CISC PUBLISHER MediaEdge Publishing Inc. 33 South Station Street North York, ON M9N 282 Toll-Free: 1-866-480-4717 ext. 229 robertt@mediaedge.ca www.mediaedge.ca Professional engineers, architects, structural steel fabricators and others interested in steel construction are invited to inquire about CISC membership. Readers are encouraged to submit their interesting steel construction projects for consideration for inclusion in this publication by contacting CISC.

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#### PLEASE RETURN UNDELIVERED COPIES TO:

Canadian Institute of Steel Construction 3760 14<sup>th</sup> Avenue, Suite 200 Markham, Ontario, Canada L3R 3T7 On the Cover: Top: The new Port Mann cable-stayed bridge. Bottom: The Simon Fraser bridge in British Columbia.



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#### By Alfred F. Wong, P.Eng. Director of Engineering



CISC provides this column as a part of its commitment to the education of those interested in the use of steel in construction. Neither CISC nor the author assumes responsibility for errors or oversights resulting from the use of the information contained herein. Suggested solutions may not necessarily apply to a particular structure or application, and are not intended to replace the expertise of a professional engineer, architect or other licensed professional.

Question 1: When only one leg of an angle tension member is attached to its end supports, with longitudinal fillet welds, how do I determine if shear lag is important and how is it accounted for?

ANSWER: The effect due to shear lag in a tension member is usually accounted for by means of an effective area method. For weldconnected members, *Clause 12.3.3.3* of CSA S16-09 applies to members of various cross sections in general. The cross-section area of the angle is divided into two components, i.e., the attached leg and the outstanding leg. Figure 1(a) shows an angle



(a)



#### FIGURE 1 — EFFECTIVE NET AREA

connected by a pair of longitudinal welds of length, L. For the attached leg, shear lag is a factor when  $L \leq 2w_2$ . In accordance with Clause 12.3.3.3 (b) (ii) and (iii), its effective net area, A<sub>n2</sub>, as shown in Figure 1(b), is determined based on the weld configuration and, for short welds, also the leg thickness. The effective net area of the outstanding leg,  $A_{n3'}$  is calculated according to Clause 12.3.3.3(c). Its shear lag effect is given as a function of the ratio of the eccentricity of the weld with respect to the centroid of the outstanding leg,  $x_i$ , to the weld length, L. Then the tensile resistance of the member is calculated in accordance with Clause 13.2(a)(iii) using the total effective net area of the angle section,  $A_{ne} = A_{n2} + A_{n3}$ .

Further information may be found in the CISC Commentary on CSA S16-09 in Part 2 of the Handbook of Steel Construction.

Question 2: I heard about the notional load requirement in the design of building structures but I cannot locate the notional load provision in the building code. Where do I find them?

ANSWER: You will find the provision for notional loads in CSA Standard S16-09, Design of Steel Structures. The Standard permits the second order effects due to gravity loads acting on the displaced structure under horizontal loads to be accounted for by using a P-delta analysis. In addition, the effects due to out-of-plumbness and partial yielding may be approximated by a set of horizontal loads, which are referred to as notional loads. The notional load to be applied at each level in addition to any other horizontal load is taken as 0.5 per cent of the concurrent gravity load acting on that level. Alternatively, a rigorous secondorder analysis that accounts for both geometric nonlinearity, including outof-plumbness, and partial yielding may be used.

Question 3: Where can I find the standard torque table for pretensioning A325 bolts?

ANSWER: The use of 'standard torque table' for pretensioning high strength bolts was discontinued several decades ago. When pretensioning is required, CSA Standard S16 recognizes three bolt installation methods:

- a) Turn- of-nut method;
- b) Using ASTM F1852 tension control bolt assemblies; and
- c) Using an F959 direct tension indicator.

Both \$16-09 and \$16-14 assign a higher slip resistance to bolts installed by the turn-of-nut method versus the other methods for a given Class of contact surface, recognizing the larger pretension typically attained using the turn-of-nut method.

Questions on various aspects of design and construction of steel buildings and bridges are welcome. They may be submitted via email to faq@cisc-icca.ca. CISC receives and attends to a large volume of inquiries; only a selected few are published in this column.



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#### By Alfred F. Wong, P.Eng. Director of Engineering

# Moment-frame connections

Following the Northridge earthquake in 1994, North American standards mandated physical testing as the basis for design of beamto-column connections in ductile steel moment-resisting frames. This requirement was adopted as an interim measure until the behaviour of these connections, particularly for welded connections, is well understood.

Extensive full-scale testing, supplemented with many analytical studies conducted since 1994, has expeditiously advanced the in-depth knowledge in ductile behaviour of several common connection types used in modern-day construction and

in improved practical solutions. ANSI/AISC 358-05, Prequalified Connections for Special and Intermediate Steel Moment Frames for Seismic Applications, a standard published in 2005, provides alternative solutions to physical testing. A similar approach is now taken in Canada. CSA S16-14 adopts the CISC publication, Moment Connections for Seismic Applications - 2nd Edition, for the design of moment connections in ductile, moderately ductile and limited-ductility moment frames, as an alternative to physical testing.

#### CISC Moment Connections for Seismic Applications -1st Edition

The 1st Edition of this CISC publication was released in 2004. The design requirements were essentially based on *FEMA 350* and conform to the limits of







A) BOLTED UNSTIFFENED END PLATE

B) BOLTED STIFFENED END PLATE

C) REDUCED BEAM SECTION

FIGURE 1 – MOMENT CONNECTIONS IN FIRST EDITION

validity established within the scope of the physical tests conducted in the SAC joint venture program. For example, frame members are restricted to rolled wideflange shapes and column depth must be within those of W360 sections. The 1st Edition of this publication incorporated the reduced beam section connection and the bolted end-plate connection, with and without stiffeners, as shown in Figure 1.

#### CISC Moment Connections for Seismic Applications – 2nd Edition

This new edition, published in 2014, adopts the design philosophy and, in principles, the design requirements incorporated in ANSI/AISC 358-10, Prequalified Connections for Special and Intermediate Steel Moment Frames for Seismic Applications. It

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## "Extensive full-scale testing... has expeditiously advanced the in-depth knowledge in ductile behaviour of several common connection types"

provides requirements that are consistent with pertinent Canadian standards, such as \$16-14 and W59-13. In addition to the connection types that are covered in the 1st Edition, it includes another field-bolted connection type, the bolted flange-plate connection, as shown in Figure 2. Other notable practical features include:

- Welded built-up sections;
- Box-shape, cruciform-shape and deep W-shape columns (See Figure 3);
- Expanded geometric validity range;
- Specific provisions for various details; and
- Designation of demand critical welds.

While the connection types included in the 2nd Edition cover most practical applications in Canada, it is not CISC's intent to restrict or discourage the use of other connection types that are proven suitable by means of physical testing in accordance with Annex J of S16-14. It should also be noted that the limitations and restrictions for their use have been adopted from *ANSI/AISC 358-10*. Connections that fall beyond the range of these limitations and restrictions but are proven appropriate by the said physical testing also conform to S16-14.

#### **Limited-ductility Moment-resisting Frames**

Although Cl. 27.4.4.2 of S16-14 provides prescriptive requirements for the design of moment connections used in *limited-ductility moment frames*, the clause applies to frames having l-shape columns and beams welded directly to the columns only. CISC *Moment Connections for Seismic Applications - 2nd Edition*, covers connections that are suitable where columns of other shapes are used and/or when fieldbolting is desired.



FIGURE 3 — COLUMN SHAPES



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# Biomimicry: Drawing design inspiration from Mother Nature

he term "Biomimicry" was popularized in 1997 by biologist and innovation consultant Janine Benyus with the publication of her book, *Biomimicry: Innovation Inspired by Nature*. The term comes from the Greek words bios, meaning life, and mimesis, meaning to imitate. So biomimicry simply means to imitate life, but more specifically it involves taking the forms and functions observed in nature and developing them into solutions for human problems.

The concept focuses on taking the 3.8 billion years of research and development that nature has been performing through evolution and adapting and applying it to real world problems. One of those real world problems is finding ways to build green and sustainable buildings. In construction, biomimicry is being used to inspire design elements in architecture, engineering better building systems and developing building materials that are stronger and more eco-friendly.

At its most basic, the practice of biomimicry encompasses three aspects we call the Essential Elements:

The **ethos** element represents our respect for, and responsibility to, our fellow species and our planet.



The **(re)connect** element reinforces the understanding that, while seemingly "separate," people and nature are actually deeply intertwined. It also represents a practice and commitment to seek out connection with the rest of nature as a source of creativity and wisdom.

And finally, the **emulate** element is learning from the patterns, strategies and functions found in nature and



## In construction, biomimicry is being used to inspire design elements in architecture, engineering better building systems and developing building materials that are stronger and more eco-friendly.

applying those lessons to inform human design.

Biomimicry is quickly gaining popularity as a leading edge, integrative approach to building design, construction and operation.

For example, photovoltaic systems, which harvest solar energy, are a first step at mimicking the way a leaf harvests energy. Research is underway to create solar cells that more closely resemble nature. These cells are water-gel-based – essentially artificial leaves – that couple plant chlorophyll with carbon materials, ultimately resulting in a more flexible and cost-effective solar cell.

Building product manufacturers are also drawing inspiration from biomimetics by studying the structure and self-cleaning surfaces of the Lotus leaf. Their research findings are driving the development of commercial coatings for selfcleaning surfaces, so they rarely have to be cleaned. Any grime that has managed to cling to a surface is simply washed away by the next rain. The materials can also be used to coat the interior of pipes, reducing clogs.

Ant colonies are being studied to understand their intricate movement patterns, and this is then used to develop integrated global logistics systems.

Additional research is underway to explore biomimetic ideas and products that have the potential to help the construction industry and its clients with demands for:

• Reduced embodied energy (CO<sub>2</sub>) in construction products;

- Reduced materials use, better resource efficiency and hence lower cost;
- Reduced weight and complexity (lighter structures, response to manual handling regulations, etc.);
- Novel designs; and
- Reduced maintenance burdens (intervals and costs).

The growing practice of biomimetic design and thinking promises to be a powerful force in shaping sustainable construction and the development of products, services, tools and resources that will help the construction industry build smarter, greener and cleaner buildings and structures in the future.

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#### INTRODUCTION



## Steel Bridges

Leveraging the performance and versatility of structural steel for building Canada's infrastructure

rom Alberta's Red Willow Bridge to the complex erection of three bridges over Toronto's Gardiner Expressway, the advantages of steel are on display in transportation structures across Canada. Combined, these projects showcase the strength and utility of one of the industry's most versatile materials, as well as that of the CISC members and associates who reinforce steel's reputation with each new build.

"CISC members are known for working on pretty sophisticated and complex bridge structures right across Canada," says Steve England, chair of the CISC National Bridge Committee and vice president of Cherubini Group. "They've also been in business for a long time, so they have the experience, they have the knowledge, and they've built a great rapport with owners, designers, general contractors and transportation agencies. That goes a long way."

CISC bridge fabricator members have left their mark from coast to coast. For this issue of *Advantage Steel*, CISC turns its attention to some of the most recent projects to highlight a portion of the steel industry's success within the Canadian construction sector. "We like to highlight our products, because we're proud of what we do," says England.

#### By Matthew Bradford

The benefits of using structural steel for bridge construction have been well documented; especially when compared to competing bridge materials. Speaking to steel's advantages over reinforced concrete, for example, CISC Solutions Centre director Alfred Wong notes steel provides more strength at a lower weight, making it an ideal choice for long spans. Using steel on remote sites also reduces the amount of material that needs to be shipped, further controlling transportation costs and related environmental emissions. Moreover, Wong notes steel's lighter properties contribute to better overall quality. "Lighter

structures attract lower seismic forces and more economical substructures," he says.

When compared to cast-in-place concrete construction, Wong adds that steel construction offers additional advantages. "Steel is typically more economical, and the fact that there is no formwork needed allows for a much faster erection, thereby minimizing traffic disruptions," he explains. "What's more, when it comes to re-decking, steel usually allows for a simpler, faster and more economical outcome."

Wong says CISC's Solution Centre research has shown steel provides for greater flexibility compared to other materials, including precast concrete girder bridges. "Horizontally and vertically curved structures preclude the use of precast concrete girders. Moreover, steel's inherent strength and stable long-term properties permit economical solutions where bridge clearance dictates a shallow superstructure," Wong explains.

Performance and durability notwithstanding, the use of steel can significantly add to the esthetic value to a project, offering designers and crews the wherewithal to create structures that not only last longer, but are more striking and pleasing to the eye. "Steel is very malleable in that sense, in that you can basically do anything you want," offers England.

The upsides of using steel in the construction of bridges are many. So too are the benefits of supporting the Canadian steel industry itself. Many of today's bridges are fabricated and produced within Canada, meaning owners benefit from reduced shipping costs while the country itself benefits from resulting economic activity and job creation. "It's important that the Canadian public know these are being built and fabricated here in Canada, so we can support jobs and our economy," says England. Read on to see just some of the bridge projects that have done their part to lift the profile of steel and CISC members on the national construction stage.



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## High capacity

#### By Andrew Brooks

Structural steel allows the City of Toronto to increase vertical clearance during the rehabilitation of three vital expressway bridges

eeping traffic moving along major expressways in a large metropolitan area is a challenge at the best of times, as any frustrated rush-hour commuter can tell you. But think of the challenge faced by those who have been given the job of reconstructing a bridge that not only crosses one such expressway, but carries a second. Then multiply the task threefold.

That was the challenge facing the project managers responsible for the complete rehabilitation of the concrete superstructures of three bridges in downtown Toronto in 2010. The bridges cross Toronto's Gardiner Expressway, the major east-west artery carrying traffic into the city's downtown

core. Two of the three bridges carry Lakeshore Boulevard West, another eastwest artery and one that is only slightly less important than the Gardiner itself.

The Frederick G. Gardiner Expressway – usually referred to as "the Gardiner" - was built in sections from 1955 to 1964. The highway has had its controversies over the years, mostly related to the elevated section of the roadway that extends from Dufferin Street, just east of the zone covered by the rehabilitation project (an area where the Gardiner actually runs below grade) eastward along the city's lakefront as far as the Don River. The use of road salt during the winter is tough on this elevated portion, necessitating expensive maintenance and frequent repair. And not all residents are happy

with its aesthetics. Over the years, proposals have been floated to upgrade Lakeshore Boulevard and eliminate this part of the Gardiner entirely, or lower it to grade, or even burv it.

Love it or hate it, Torontonians heavily depend on the Gardiner, one of the city's busiest thoroughfares. Everyone Advantage Steel spoke with about the project agreed that traffic management was the most significant challenge they faced. And since two of the bridges carry Lakeshore Boulevard West's westbound lanes, it was here that traffic management was the real issue. These lanes carry an annual average daily traffic volume of more









than 29,000 cars – a bit over 9,800 for each lane. Volume usually peaks in the afternoon rush hour, with around 3,000 vehicles an hour.

In 2010 the City of Toronto determined that the concrete superstructure of all three bridges had deteriorated to the point that it was beyond feasible repair. The only alternative was reconstruction. The city chose AECOM as the consulting engineer for the project.

AECOM's Srdjan Brasic, project manager for the job, says that concrete was considered for the new superstructures before structural steel was chosen. Steel won out, he says, in part because of its suitability for one of the project's other objectives.

"The city wanted a shallower structure in place than what was there previously," Brasic says. The existing vertical clearance over the Gardiner was within the legal requirements, of course, but the city wanted to take the opportunity to increase it. "We looked at other types of structures but found that we could only get that improved clearance by using steel."

Brasic says that alternative materials would have required changing the geometry of the Gardiner's road surface. That was far beyond the scope of the bridge rehabilitation project and would have amounted to an entirely different project of tremendous scope that involved huge difficulty, expense and disruption of traffic.

A number of traffic management options were considered, and in the end it was decided to create a temporary three lane detour for the westbound Lakeshore, starting at the intersection of Lakeshore and British Columbia Road and

#### The Bridges:

- Bridge 009 (two spans) carries Lakeshore Boulevard West's westbound lanes from the south side of the Gardiner Expressway to the north side, at Dunn Avenue.
- Bridge 008 (two spans) lies between the other two and carries Jameson Avenue's northbound and southbound lanes over the Gardiner to meet Lakeshore Boulevard West's eastbound lanes, which run south of the Gardiner. (Lakeshore Boulevard West's westbound and eastbound lanes are separated where they run through the project zone.)
- Bridge 006 (four spans) carries Lakeshore Boulevard West's westbound lanes from the north side of the Gardiner back to the south side, just west of Jameson Avenue.







ending just west of the wing walls of the Jameson Avenue bridge (Bridge 006). The total detour length was around 800 metres. A temporary intersection at Jameson Avenue and Lakeshore eastbound and westbound, complete with temporary traffic signals, was also constructed.

The project got underway on May 1, 2010. While high priority was assigned to minimizing traffic disruption, the Gardiner did have to be completely closed over three weekends to allow the demolition of the existing reinforced concrete superstructures. Otherwise, the expressway was reduced to two of three total lanes. During erection of the steel girders the Gardiner had to be completely closed in a single direction at a time. These closures were timed as much as possible to non-peak hours.

"The most challenging constraint to the steel erection was that the Gardiner Expressway had to remain open for two lanes in each direction except for a very limited number of planned closure weekends," says Clyde Crocker, P. Eng., project manager for Soncin Construction, the construction company on the project. "As such, field splices had to be designed so that the splice locations occurred in laneclosed areas wherever possible."



Steve Matthews, division manager, Structural Steel and Bridge Division for E.S. Fox Ltd., the Niagara Falls-based erector, also says that maintaining traffic flow on the two busy roadways was the primary challenge during construction. Matthews particularly commends the work of Soncin Construction in managing the overnight road closures that enabled the erection work to go smoothly. "Soncin was great to work for and they performed their own road closures," he says. "This was a big part of the success of the project."

The girders were fabricated by Mometal Structures Inc. in Montreal. "The taper in the girders, their length and transport, were among the distinguishing features of this job," says Mometal president Joseph Ciccarelli. "But none of that presented any particular challenge for us. It's actually more on the simple side of the work we do. We aren't set up to do volumes of any one thing – the more things are off the beaten path, the more value we can bring to a job."

Getting the completed steel pieces to the work site required fabricating the girders in smaller sections that could be field spliced once onsite. The success of the onsite field splicing was ensured What will you get hit with today? A bunch of rookies? Or a Lost Time Accident?

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by shop matching of the girders before delivery, Ciccarelli says. As well, the onsite areas where the splicing took place were outside active traffic lanes, which also made the job easier.

"Some items that I presented at the time of tender were to make the girders longer and eliminate some of the splices shown on the bid drawings," says Steve Matthews. "This did happen for the Jameson bridge and the Dunn and Lakeshore structure (Bridge 009)."

Between four and eight girders could be erected a night, depending on how many cranes were in operation. "It was a very short window over the highway for crane assembly, steel erection and crane dismantling," Matthews says. "Staging girders and preparing the splices, installing the fall arrest system, etc., were all done ahead of time to ensure the least amount of time required during the closure." Shop-welded lifting lugs were added to the girders to speed erection.

Soncin was able to complete the closures, which covered the 12 a.m. to 4 a.m. window, in 15 minutes. "We'd have the cranes and girders prepared and ready to roll out onto the closed Gardiner," Matthews says. "The cranes would be prepared prior to the closure to ensure they were ready to work in the configuration required. The crane placement and erection procedures were all engineered by our engineer George Paul."

The precision of these operations was a huge contributor to the eventual success of the project. Work was mostly completed on July 28, 2011, six months ahead of schedule, and within the \$14.5-million project budget. That's an excellent result for any project, public or private sector.

#### Increases in vertical clearance in metres

Bridge	Previous	New
Bridge 009 (at Dunn Ave.)	4.58	5.29
Bridge 008: (Jameson Ave.)	4.69	5.15
Bridge 006: (west of Jameson Ave.)	5.33	5.35
ICourton AECONAL		

(Courtesy AECOM)



#### Design and fabrication details

_		Total tonnes	Girder	<b>Field splices</b>
Bridge	Spans (metres)	(mega gram)	segments	per girder
Bridge 006 (Lakeshore Blvd. west of Jameson)	Four spans: 20.3m, 34.1m, 34.1m and 20.3m	370	7	4
Bridge 008 (Jameson Avenue)	Two spans: 22.4m and 22.4m	148	9	2
Bridge 009 (Lakeshore Blvd. at Dunn Ave.)	Two spans: 25.9m and 27.4m	157	7	2

(Courtesy AECOM)





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## Restoring Red Willow River Bridge

Implementing an orthotropic steel deck solution ensures an efficient bridge rehabilitation

Eric Levesque, ing., M.Sc. & Yannick Martin, ing. jr.

tructal-Bridges took the initiative and proposed a lightweight solution to Alberta Transportation in order to rehabilitate the Red Willow River Bridge in Northwestern Alberta. As the existing concrete deck of the three-span bridge reached the end of its service life, Alberta Transportation looked for an economic solution for its rehabilitation and considered Structal-Bridges' proposal to be appropriate. Therefore, Structal-Bridges brought technical support to the engineering firm Focus located in Edmonton to develop the preliminary concept for an innovative orthotropic steel deck solution. Alberta Transportation decided to move ahead with the concept: Focus and Roche then performed the detailed engineering of the project.

#### **Orthotropic Steel Deck**

Orthotropic steel decks (OSD) used in bridge applications are basically made of a large deck plate, stiffened on the underside by transverse floorbeams and longitudinal members, namely the ribs and the inverted Ts. Components are manufactured and welded together into several transportable prefabricated panels that can be easily brought on-site and rapidly erected for bridge construction as well as bridge rehabilitation projects.

#### Design

The system is fabricated with corrosion-resistant steel plates. Comprehensive finite element analysis has been carried out to ensure that all the fatigue details meet the requirement of Canadian Standards CSA-S6-06 for Class-B roadway with two design lanes and CL-800 design vehicle. Traffic barriers with PL-2 performance level are mounted on the side of the deck with bolt-through connection.

Although the concrete deck of the Red Willow River Bridge has to be replaced, the good condition of the existing longitudinal steel girders allowed for their reuse. The OSD system was designed to be attached to the girders with slipcritical bolted connections in order to develop full composite action in the superstructure and increase the live load capacity of the girders. The efficient use of steel material within the components of this OSD configuration leads to a lightweight structure. While the width of the bridge deck has been increased from 7340 mm to 8940 mm (with 1156 mm deck overhang), the overall mass of the deck has been reduced from approximately 283 to 168 metric tons, which represents a 36 per cent mass reduction. This



FIGURE 1: 3D MODEL BUILT BY STRUCTAL-BRIDGES' DRAFTING TEAM

weight saving allowed for the bridge to withstand the actual traffic loads without replacing or reinforcing the existing girders, which results in significant economic benefits on the overall cost of the project.

#### **Fabrication**

Shop drawings have been produced from a 3D model built by Structal-Bridges' drafting team (Figure 1), based on the engineering plans. Shop programs are created from the model and are numerically imported into CNC machines for cutting and drilling operations, so the parts are fabricated as modelled. From the machining of the first components to the final assembly of the deck,

#### Steel as the best solution

Dominique Blouin, construction and business development manager at Structal-Bridges, comments on the choice of building material

"Structal's orthotropic steel deck solution used on the Red Willow Bridge project was the best solution for this two-lane bridge. It is the perfect product for a quick deck replacement over existing girders. Contrary to a conventional concrete deck, this replacement can be performed even in harsh winter conditions while allowing for traffic on the second lane. This deck is easy to install using only conventional steel erection equipment. Studies performed over the last decades have led to North American specifications that support well the design and fabrication of an orthotropic steel deck. That research improved critical welding details as well as quality control procedures which will enhance deck performance and allow it to be designed for a 75-year lifespan. Structal-Bridges is proud to be part of this project."



#### **RED WILLOW BRIDGE**



FIGURE 2: LONGITUDINAL RIBS BEFORE THEIR ASSEMBLY ON THE DECK PLATE



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the fabrication is carried out efficiently by a qualified workforce supported by competent professionals.

Assembly of the ribs to the deck plate is performed with an 80 per cent partial joint penetration, one-side submerged arc welding. The success of this challenging step for the fabricator is ensured with a rigorous quality insurance program on the parts dimensions and pre-assembly. Competent welders work with reliable equipment and well-tried welding procedures. For this particular step, Structal-Bridges proposed an alternative method to achieve efficient and rigorous quality control of the partial joint penetration weld. With design engineer's approval, quality control is managed with 100 per cent phased-array ultrasonic testing (PAUT), an advanced inspection method that allows for accurate monitoring of the penetration on the full length of the weld. Quality control of all the other welds is achieved either with ultrasonic testing (UT), magnetic testing (MT) or radiography testing (RT).

Longitudinal inverted Ts and transverse floorbeams are subsequently assembled within the panel. Welds are carefully executed at the intersection of the structural components. Based on the AASHTO code, some standard practices of the industry in Canada have been adjusted to OSD fabrication in order to produce enhanced fatigue-resistant weld details. Structal-Bridges proposed adapted details to design engineers and good communications between the stakeholders of the projects led to rapid acceptation of the proposed details.

A thin layer of polyurethane-based wearing surface is shop-applied on the orthotropic panels. Bimagrip LS, a product of RS Clare & Co Ltd, was picked for the project. While the standard bridge design of Alberta

#### **RED WILLOW BRIDGE**

would have a dead load of 7.3 kPa, the OSD/Bimagrip solution will weigh 2.9 kPa, representing only 40 per cent of the standard bridge design dead load. RS Clare offered a 10-year warranty on its wearing surface, ensuring a longterm high-quality product to the bridge owner.

#### **On-site installation**

On-site operations are scheduled from June to October 2014, including the removal of the existing deck, replacement of the bearings, repairs of the abutments, surface preparation of the main girders and installation of OSD panels. The construction sequences have been staged so that the bridge remains open to a single lane of traffic at all times in order to minimize traffic disruption during the rehabilitation.

In conclusion, bridge owners have a growing interest in OSD construction, especially because of the tremendous potential related to this cost-effective and rapid bridge rehabilitation solution. Structal-Bridges has the expertise to work with bridge owners and engineering firms to develop adapted bridge solutions for a wide range of applications, either for rehabilitation or new construction. The rehabilitation of the three-span bridge over Red Willow River has provided an opportunity to confirm the reliability of orthotropic steel deck projects and to promote the innovative use of a product that is already well known worldwide in the steel industry for design and construction of bridges. The industry and Structal-Bridges are proud to have contributed to the success of this project by providing an innovative solution adapted to client and road user needs.



FIGURE 3: WELDING OF THE TRANSVERSE COMPONENTS OF AN ORTHOTROPIC PANEL

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#### The fabrication perspective:

The 70-metre-long Red Willow River Bridge consists of three spans supported by four existing steel girders. Its rehabilitation

#### The owner perspective:

The existing reinforced concrete bridge deck on the Red Willow River Bridge was experiencing regular failures and was in urgent need of replacement. Alberta Transportation wanted a wider deck to match the width of the adjoining involves the fabrication, delivery and installation of eight orthotropic deck panels of 72 m<sup>2</sup> each, for a total steel weight of 168 metric tons.

roadways and a thicker concrete deck to improve its capacity and durability. Preliminary investigations found that the existing girders and substructure were already at or very near their load carrying capacity and would not support a wider, thicker Shop-applied thin wearing surface contributes to a lightweight solution and reduces onsite work as well as traffic disruption.

concrete deck without strengthening. An orthotropic steel deck proved to be the ideal solution, providing a lightweight, full-width deck that not only reduced the dead load of the structure, but increased the loadcarrying capacity of the girders.

#### Structural analysis and technical considerations

#### Loads absorbed by the deck:

The dead weight is absorbed by the deck without composite action, given the presence of the weight before bolting the orthotropic deck. The live loads coming from road traffic loads are absorbed by the deck in composite action.

#### Modelling:

The deck was modelled by a trellis, including all the longitudinal and cross members, the troughs and the upper deck plate. Two-dimensional plate elements were used to simulate bidirectional action during the passage of truck wheels. Finally, a more specific finite element analysis was performed for the details and the more critical and fatigue-sensitive elements.

#### Design characteristics:

Life cycle for fatigue analysis purposes – 25 years. The fatigue analysis of an orthotropic deck is critical, especially at the junction of the troughs with the cross members. As indicated below, 14 critical locations were analyzed more attentively.

#### Field adjustment details:

Since a vertical field adjustment is required to ensure the assembly of the orthotropic deck with the existing longitudinal beams, a system of adjustable angle brackets was developed instead of the traditional inverted T-beam. See the figure below.







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#### PORT MANN BRIDGE



FIGURE 1: PORT MANN BRIDGE HWY 1 PROJECT LAYOUT

## Expanding a Vancouver centrepiece

The Port Mann Cable-Stayed Bridge into Vancouver is widened to 10 lanes as part of the province's Gateway Program

By David Goodyear, P.Eng.

The Port Mann Bridge Highway 1 project was tendered in 2007 as part of the Gateway Program in Vancouver, B.C. The project was part of the B.C. government's program to upgrade the transportation network in the Vancouver Region in order to ease congestion on Hwy 1.

The scope of the project included upgrading approximately 37 kilometres of highway, including the existing bridge crossing of the Fraser River (Figure 1). The project called for doubling the capacity over the river, expanding the five-lane facility to 10 lanes.

**The project:** The new Port Mann Bridge is the centerpiece of, and the tollgate for, the major redevelopment of Highway 1 crossing the Fraser River into Vancouver. The scope and complexity of the project make it one of the most ambitious highway transportation projects in North America. The form of delivery makes it even more impressive in that the entire development was tendered as a private concession. The instructions to proposers called for a privately financed development with a 40-year concession that included the time of construction. The Request for Proposals (RFP) for this massive project included 28 schedules covering every aspect of procurement, design, construction and operations, setting forth the terms and processes for a comprehensive development program.

Selection of the preferred proponent was based on submission of the best net present value (NPV) of the annual concession payments proposed for the development among those who submitted a compliant technical proposal. The Connect BC Team, led by Macauarie as concessionaire, with Kiewit Flatiron General Partnership (KF) as the DB contractor, and with TY Lin International leading the Fraser Crossing design and Hatch Mott McDonald-MMM (H5M) leading the on-shore design, was selected as the preferred proponent.

In the time between selection of the preferred proponent and financial close for the project, the financial markets retracted to the point where the financial plan tendered for the project was in jeopardy. The B.C. government stepped in to address the financial crisis by having the corporation TICorp assume the role of concessionaire. The project then advanced to closing, and a contract was signed with the design-builder KF in March, 2009.

Project development: For the Fraser River Bridge, the Reference Concept called for upgrading the existing bridge, and building an five-lane adiacent cable-stayed bridge to provide the required 10 traffic lanes. The original Port Mann Bridge was a record-setting 366m main span deck tied arch, with the balance of the two-kilometre crossing comprised of plate girder approaches. The old bridge had stay in service throughout to construction of the new facility.

**Bridge type studies:** Evaluation of alternatives for the new Port Mann Bridge was led by the KF team with the goal of developing the best net present value alternative for the project. The RFP included a number of restrictions on alignments and pier locations, most notably that one could not have a pier on the south bank of the Fraser River, adjacent to the pier already on the south bank for the old bridge. With the 470-metre main span then needing to cross the CN rail yard on the south, the focus quickly moved to cable-stayed alternatives.

The initial screening study of alternatives focused on the Reference Concept for keeping the old bridge and constructing a new five-lane structure. The assessment of maintenance and financial risk associated with extending the old bridge for another 40 years trended towards the merit of a total replacement.

There were two choices for fitting 10 new lanes in a five-lane corridor. One was to develop a double deck solution with an over-under fivelane arrangement. The second was to develop a single level, very wide deck system to carry all 10 lanes. While the double deck configuration itself was not difficult, the transition from a double deck to a single deck approach would be quite expensive. In the case of the Port Mann site, the roadway braid needed for the approach bridge to the southern side required significant extension of the bridge, expensive substructure and



complex geometrics for the roadway and approach. A single, central pylon section was developed in order to have tower foundations fall within the Reference Concept rightof-way and allow construction to advance adjacent to the operating bridge (Figure 2). A steel superstructure was ideal for this span and configuration, since deck weight for a composite steel section is considerably less than for a concrete alternative.

The single central pylon concept would support both a two-stay plane full width section and a twin deck fourstay plane section as steel or steel composite deck sections. Sections were developed for both full width steel truss. floorbeam or box section and for a twin composite edge girder section. The steel quantity for a twocable plane system was approximately 35 per cent greater than for a fourplane system due to the longer floorbeam span. Each of the twin composite frame sections was fairly conventional, and similar to many single four and six lane cable-stayed deck structures built in North America (Figure 3).





ELEVATION

FIGURE 2: NEW PORT MANN BRIDGE LAYOUT

#### **Details of design**

**The framing system:** Each of the two deck frames was a standard floorbeam and edge girder system. However, there were several non-standard aspects of the framing layout associated with the central tower.

1.The constraints of the layout described for the type selection included an atypical span layout. While the railroad yard affected the main span layout, the back spans were constrained by the definition of a secondary navigation channel on the north. The resulting backspan ratio was .4 of the main span, which is less than optimum for girder and anchor pier design on a highway bridge, requiring a large tie-down detail for the anchor piers.



#### Main Span Typical Section

FIGURE 3: MAINSPAN COMPOSITE DECK SECTION

#### Port Mann Bridge main span

Canron Western Constructors LP live up to the challenges

Canron Western Constructors LP was awarded the supply of the main span structural steel for the new Port Mann Bridge in 2009. This new bridge Is a balanced cantilever scheme, which means that the erection started at both the south and north towers. Panels were added alternating from one side to the other until the two fronts met in the mid span over the river.

Canron also supplied the sidewalk framing, wind fairings, damper, restraint and tie-down units. The fabrication supply represents over 240,000 shop hours that were shared between the Annacis, Delta and Portland plants. Each of the 272 cable stay anchor units is slightly different than the other based on the fact that the bridge has camber, and the slopes are different from the north and south and side to side. They are an extremely complex component of the bridge requiring stringent geometry controls as well as complicated welding conditions.

One of the other major challenges on this project was the fabrication of the eight heavy edge girders that sit on the abutments. These girders are 24 metres long, very complicated and weigh 110 tonnes. The ends of these girders are fracture critical, and to weld the thick flanges, web collars and stiffeners required a very elaborate preheat system to be used to control the duration of cool down. The welding (around the clock) and testing to the American 01.5 code were a challenge to the shop tradespeople.

#### Quantities:

Main edge girders (four across): 252

Floor beams: 394 Cable stay anchors: 272 Median struts: 62 Top flange bracing: 432 Temporary bracing: 780





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#### Inclined Cable Plane 3D Schematic







- The offset of deck relative to the tower resulted in splayed cables emanating from the single towerhead. The frame included struts between each deck to balance the resulting horizontal cable force across the width of the bridge.
- In order to allow lanes from the main spans to meet an economical 3-box frame in the approaches, the backspan frames were tapered

towards each other. This was only practical with the central pylon scheme.

4. The width of the single central tower was limited by the available right-ofway at the south pylon, and would affect the cost of framing across the inter-roadway gap. The narrow section had limited lateral strength as a freestanding pylon. So the lateral system was also designed as a stayed system, with transverse stabilizer stays connecting the base of the towerhead to stabilizer beams emanating from the tower. The resulting stay system created a cable-stayed pylon that was similar in concept to a sailboat mast, allowing a slender pylon section to work as a pure column instead of the more typical bending mode of a portal frame.

5. The truck clearance required a taller tower for minimum roadway clearance to the stay plane. The tower height was increased approximately 12 metres for this condition.

Deck cable anchors: Deck anchorages for composite steel cable-stayed bridges generally follow one of two forms - fin anchors above deck (extensions of the edge girder web) or bucket anchors below deck (attachments to the side of the edge girder). For the more typical framing systems, these deck anchors are both regular in geometric configuration, and either vertical or only slightly splayed against the vertical frame. The wider offset associated with the fourplane, 10-lane structure resulted in both irregular geometry and considerable lateral cable angles for deck anchorages.

We investigated three basic configurations for these deck anchors. These were:

- 1. Fin anchors with bent web plates above the deck;
- 2. Fin anchors with canted edge girder geometry; and
- 3. Bucket anchors with bolted anchorage assemblies.

#### PORT MANN BRIDGE

One aspect of splayed stay geometry is that the lateral cable angle of the stay plane is not in the vertical plane (Figure 4). Cable sag, and change in cable sag with changing stay force and vibration, follows the vertical plane. For the typical roadway geometry, the difference in these angles from vertical is slight. But as the offset gets larger, so does the lateral component associated with the difference in vertical cable sag vs. lateral stay plane angle. These conditions affect anchor stiffness, damper performance, fabrication and inspection requirements (Figure 5). The bucket anchor configuration was selected for its superior outof-plane stiffness and associated damper performance.



**FIGURE 5: BUCKET ANCHOR** 

#### **Steel erection**

For those who like variety, the erection planning program was an ideal assignment. And with two major bridge contractors on the same team, there was no shortage of experience and ideas for erection.

The south cantilever had to deal with limited access over the railroad and over-water erection for the main span, but had an open field for erection of the south backspan. The north cantilever was all over water. The logistics of the south backspan required that erection be fed from outside the railroad yard. So direct lifting by derrick in the standard fashion was not practical. In addition, the heavy weight of the



FIGURE 6: GENERAL ERECTION LAYOUT



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#### PORT MANN BRIDGE



FIGURE 7: NEW PORT MANN CABLE-STAYED BRIDGE

first field section at each backspan pier was more than a typical deck mounted derrick would handle. The over-water access for the north cantilever permitted lifting a fully assembled steel section. Three separate erection methods were adapted for steel erection. In addition to the gantries used for the north cantilever, derricks were used for stick erection of the south main span, with crane erection for the south backspan (Figure 6).

The more challenging control for steel frame erection is generally the lateral drift, since typically there is nothing in the permanent frame to adjust alignment. That challenge was amplified for the twin barrel deck system on Port Mann. In order to avoid sidesway, the two deck frames had to be erected in parallel. Should they get out of line, there would be a time consuming and challenging process to pull two decks back in line at the same time if drifts differed between the two. So, as we started erection, the number one objective was to hold alignment throughout assembly. The erection crew's diligence paid off, for the alignment during erection was better than any we have seen on even simpler bridges.

In summary, the Port Mann Highway 1 development project was tendered on the basis of a best value defined as the lowest net present value cost over the operating period for technically compliant alternatives. The project development by the successful proponent led to a twin roadway steel composite cablestayed bridge solution based on the economic advantages in cost, schedule and maintenance, which, when blended with operating factors, produced the lowest net present value offering to the owner (Figure 7).

#### **Credits:**

**OWNER:** Transportation Improvement Corporation, a B.C. Crown Corporation

ORIGINAL CONCESSIONAIRE FOR TENDER: Macquarie Infrastructure

**DESIGN-BUILDER:** Kiewit Flatiron General Partnership

HIGHWAY AND CIVIL DESIGN: H5M, a joint venture of Hatch Mott McDonald and Marshall Macklin Monaghan

**BRIDGE DESIGN:** T.Y. Lin International in collaboration with International Bridge Technologies

#### **STEEL FABRICATION AND SUPPLY:**

Canron Western Constructors, Vancouver B.C.; Oregon Iron Works, Clackamas, OR

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For the full course schedule, information, online registration and the latest updates, please visit our website at www.ciscicca.ca/courses, or request a copy of our course calendar.

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The course will also touch upon the steps involved in an investigation and evaluation in issues of design, manufacturing, fabrication, erection and inspection. As the industry and projects tend to be litigation orientated and are in constant dispute, the course will incorporate a roundtable discussion and summary of the above and assessment of responsibility, risk management, and recommendations avoidance of issues.

Of interest to chief building officials, building inspectors, plans reviewers, architects, engineers, field inspectors, building envelope consultants, fabricators, erectors, project managers, general contractors and owners.

Course Leader:
Joseph (Joe) S. Vidican, P.Eng., Principal, Vidican
Engineering (Building Science & Forensic Engineering)

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Winnipeg, MB	Nov. 10		1

#### **Connections for Design Engineers**

This course is intended to provide practical guidance to steel designers and clarify the complementary roles of the fabricator and the design engineer with respect to connection design. Emphasis is placed on connections and their impact on costs and economy.

The basic objective is to assist designers in their understanding of how connections influence member design and vice versa, and to emphasize the importance of considering both connections and member selection for optimum economy. The scope of the course is limited to connections normally encountered in common types of steel building structures.

The presenters will highlight major changes in \$16-09 that influence the design of structural steel connections. Topics include high strength bolts, welds, bolts in tension and prying, slip-critical connections, welds and bolts in combination, eccentric connections, simple shear connections, seated beam connections, connection to concrete, column connections, moment connections (W & HSS Sections), bracing connections, gusset plates and truss connections.

Course Leaders:

John R. Mark, M.Sc., P.Eng., Past President, M&G Steel Ltd Peter C. Birkemoe, Ph.D., P.Eng., Professor Emeritus, University of Toronto

Halifax, NS	Sept. 16	Calgary, AB	Sept. 18
Ottawa, ON	Sept. 17	Vancouver, BC	Sept. 19

#### **Industrial Building Design**

This course is intended to provide understanding on design theory and the rationale behind code provisions that are unique to steel-framed industrial buildings. It focuses on practical and economical solutions for framing a typical industrial building to the requirements of the 2010 National Building Code of Canada and the pertinent provisions of CSA Standard S16-09.

The learning goals for this course include the following: identify the unique environmental and mechanical loading conditions in industrial buildings, learn the applicability and limitations of current codes and standards in Canada, select the most cost effective framing schemes, design crane-supporting girders, stepped columns, purlins and girts, explore lateral force resisting systems, roof trusses and efficient connections, understand serviceability considerations and limitations, design for high and low temperatures, learn the implications of seismic provisions, plus other topics such as fatigue, standing seam roofs, rehabilitation, tolerances and coatings.

Course Leaders:

Robert A. (Bob) MacCrimmon, P.Eng., Senior Civil/Structural Specialist, Hatch

Logan Callele, M.Sc., P.Eng., Engineering Manager, Waiward Steel Fabricators

Toronto, ON	September 23
Saskatoon, SK	September 24
Calgary, AB	September 25

#### Single Storey Building Design - New Online Course -

This course focuses on practical and economical solutions for framing a single storey warehouse building with attached office area to the requirements of the 2010 National Building Code of Canada and the pertinent provisions of CSA Standard S16-09.

Practical steel framing concepts and integration with architectural and mechanical features will be discussed. The presenters will highlight major changes in NBCC 2010 and CSA S16-09.

Topics include ponding of rainwater, snow drifting, companion load combinations, wind and seismic loads, notional loads, P-delta effects, selection of deck and joist systems, design of

Gerber girders, design of interior and exterior columns, girts, base plates and anchor rods, selection and design of braced frames and roof diaphragm, fire protection issues, steel fabrication considerations, material selection and economics.

Course Leader:

R. Mark Lasby, B.Sc., P.Eng., Principal Structural Engineer, Fluor Canada Ltd., Calgary

Webinar Format (4@2hrs)

Nov. 5-6, 12:00 - 2:00 p.m. and 3:00 - 5:00 p.m. ET

### Inspection of Steel Building Structures - Accreditation Program -

This 3½-day course will prepare inspectors, designers, building officials, fabricators, erectors and other specialists for the inspection of steel-framed buildings in the field. A course participant who achieves an 80 per cent grade on the optional three-hour final exam on the final day will be designated by CISC as an Accredited Steel Inspector - Buildings.

Applicable sections of the National Building Code of Canada, CSA S16 plus referenced material, product and quality standards, CISC Code of Practice and CISC Certification guidelines will be addressed. Typical structural, erection and shop drawings for steel-framed buildings will be explained. Material identification, tolerances, bolting and welding processes and procedures will be reviewed. Included are OWSJ, floor and roof deck, shear studs, surface preparation and coatings.

Course Leader:

Robert E. Shaw, Jr., PE, President, Steel Structures Technology Center, Inc.

Toronto, ON - 1:00 p.m., Oct. 6 to 12:00 p.m., Oct. 10

#### Inspection des structures de bâtiments en acier - Nouveau cours : Programme d'accréditation -

Ce cours de 3 ½ jours préparera inspecteurs, concepteurs, agents du bâtiment, fabricants, monteurs et autres spécialistes à inspecter sur le terrain des bâtiments à charpente métallique. Un participant qui obtient une note de 80% à l'exam final facultatif de 3 heures offert la dernière journée sera désigné par l'ICCA comme un inspecteur accrédité – bâtiments en acier.

Les sections applicables du Code national du bâtiment du Canada, la norme CSA S16 ainsi que le matériel référencé,

les produits et normes de qualité, le Code pratique standard de l'ICCA et les lignes directrices de certification de l'ICCA seront abordés. Les dessins typiques de structure, de montage et d'atelier pour les bâtiments à charpente d'acier seront expliqués. Les processus et les procédures d'identification du matériel, des tolérances, du boulonnage et le soudage seront examinés. Les poutrelles, le tablier de plancher et de toit, les goujons de cisaillement, la préparation de la surface et des revêtements sont inclus.

Conférenciers: À confirmer

Montréal, QC	Février 2015
Québec, QC	Février 2015

#### Nouveautés CSA S16-09 et survol du Handbook - Webinaire -

Ce cours traite des modifications apportées à la norme CSA S16-09 et au dimensionnement des charpentes métalliques à l'aide de la 10e Édition du « Handbook of Steel Construction ».

Ce cours est proposé en ligne, en quatre séances de deux heures, via le système GoToWebinarMC. Les personnes intéressées peuvent s'inscrire aux quatre séances (0,8 UFC/ CEU seront accordés à la fin du cours), ou à la séance unique sur la norme CSA S16-09 (0,2 UFC/CEU seront accordés à la fin du cours). De plus, des offres de remise groupées avec le « Handbook » et l'adhésion à l'ICCA seront proposées aux participants lors de l'inscription.

Le cours de formation continue de l'ICCA, Nouveautés CSA S16-09 et survol du « Handbook », est présenté en ligne (webinaire) en quatre séances de deux heures comme suit.

#### Conférenciers:

Hellen Christodoulou, Ph.D., ing., B.C.L., LL.B., M.B.A., Directrice Régionale-Québec, ICCA Charles Albert, M.Sc.E., P.Eng., Directeur des publications techniques, ICCA

12 novembre 12 h - 14 h et 15 h - 17 h (HAE)

13 novembre 12 h - 14 h et 15 h - 17 h (HAE)

### Conception, fabrication et construction de ponts en acier

Ce cours traite de la conception, de la fabrication et de la

construction de ponts en acier selon la norme CAN/CSA-S6-06, Code canadien sur le calcul des ponts routiers, supplément no #1. Ce cours a pour but d'aider à mieux comprendre la théorie de conception et le raisonnement des dispositions du code ainsi que l'application de certaines formules et exigences du Code. Les aspects pratiques et économiques de la fabrication, du montage, du choix des matériaux et leurs conséquences sur la conception seront également mis en évidence.

Conférenciers:

Gilbert Grondin, Ph.D., P. Eng., Senior Bridge Engineer, AECOM & Adjunct Professor, University of Alberta Jean de Gaspé Lizotte, M.Sc., ing., Directeur, Projets spéciaux, Dessau Soprin inc. Richard B. Vincent, B.Eng., ing., Vice-président, recherche, Groupe Canam Inc.

Montréal, QC

25 et 26 novembre

#### **EVENTS**

#### SASKATCHEWAN REGIONAL MEETING

Come to our Saskatchewan Regional Meeting on June 25 at the Best Western Royal Inn.

#### ALBERTA REGIONAL MEETING -BLACKHAWK GOLF CLUB

Alberta has a regional meeting that we would love for you to attend. Come to Blackhawk Golf Club on August 11, and we can play golf after to connect with members and associates.

#### SASKATCHEWAN GOLF TOURNAMENT

Saksatchewan has a golf tournament on September 12, 2014. Come and play golf with us at Moon Lake Golf and Country Club.

### 2014 CISC 85TH ANNUAL CONFERENCE & NATIONAL DESIGN AWARDS

Join us for three exciting days of networking and social events, dynamic presentations and a taste of Atlantic hospitality! Reserve your hotel room for October 1 to 3, 2014.

#### SAVE THE DATE: 6th ANNUAL QUEBEC STEEL WORKSHOP

Quebec Steel Symposium & Trade Show and Quebec Steel Industry Awards of Excellence

The contribution of the steel industry to the world of transport and infrastructure, on October 3, 2014.



# September 19, 2014 is **STEELDAY**

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#### New Members and Associates

CISC welcomes the new members and associates approved by the board:

#### **Fabricators**

Imperial Metal Industries Inc., Blumenort, MB Acier Profilé SBB Inc., Terrebonne, QC Hopkins Steel, Welland, ON

#### **Associate Consultant Companies**

DTI Structural Engineers Inc., Tecumseh, ON SKC Engineering Ltd. (welding engineering), Surrey, B.C. Pharaoh Engineering Ltd., Medicine Hat, AB John G. Cooke & Associates Ltd (Consulting engineers), Ottawa, ON AMEC Americas Limited, Vancouver, B.C. AMEC Americas Limited, Saskatoon, SK Protostatix Engineering Consultants, Edmonton, AB

Associate Suppliers Park Derochie, Edmonton, AB Aarc-West Industrial Coatings Inc., Surrey, B.C. Aggressive Tube Bending Inc., Surrey, B.C. Canadian Quality Inspections Ltd., Winnipeg, MB

Associate Technical Individuals Firas Shaker, Self-employed, Baghdad University, Civil Engineering, Oakville, ON

#### **Associate Professionals**

Frédéric Marquis, P.Eng., OIQ, Pasquin St-Jean & Associés, Montreal,QC Eric Boudreau, P.Eng, PENB, Senior Civil/Structural Engineer, Rally Engineering, Fredericton, NB Remo Rinadli, P.Eng., OIQ, Bridge Engineer, Canadian National Railway, Montreal, QC Brian Waddell, P.Eng, PEO, Structural Engineer, Waddell Engineering Ltd., Cambridge, ON Bram Toomath, P.Eng, Hannigan Engineering,

- Vaughan, ON
- Joseph Vidican, P.Eng., Vidican Engineering Inc., Belle River, ON

David D. Perry, P.Eng, Civil/Structural Engineer, DMG Consulting Ltd., Gander, NL

Rory A. Smith, P.Eng., Structural Engineer, Stantec, Calgary, AB

**Associate Steel Erectors** Ramco Installation Ltd., Stoney Creek, ON St. Peter Steel Inc., Brampton, ON

#### Associate Fabricators

Acier Charron Ltée, Boisbriand, QC Coquitlam Steel Products Ltd., Port Coquitlam, B.C.

2014 Joint Architectural and Engineering Educators' Meeting The CISC Quebec Region was the host for the 2014 Educators' Conference, which was held from February 28 to March 1 in Quebec City.

This two-day gathering of architectural and engineering professors who teach steel design and construction at Canadian universities has been held biennially since 1985. The goal of the meeting is to renew the educators' enthusiasm for steel construction, provide updates on new trends in the industry, give them an opportunity to network and discuss educational issues, and to set the stage for greater collaboration and sharing of knowledge and resources.



Networking at the 2014 Educators' Meeting in Quebec City

2014 G.J. Jackson Memorial Fellowship Award The G.J. Jackson Fellowship is awarded annually by the Steel Structures Education Foundation in memory of the late Geoffrey Jackson. Jackson was, for many years, a leader in the Canadian structural steel fabrication industry and was a founding member of the Steel Structures Education Foundation. The award is presented to Canadian engineering students conducting graduate studies in structural engineering, with major emphasis on steel structures. This prestigious award is currently valued at \$20,000 over a one-year period. This award is presented at the Annual SSEF – CISC Convention and commemorated at the Annual SSEF – CISC Convention and commemorated with the Geoffrey J. Jackson Memorial Certificate.

The 2014 Jackson Fellowship recipient is François Leprince, a master's candidate who is studying at Université Laval under the supervision of Professor Josée Bastien.

Leprince is conducting research on the "Study of Resistance to Fatigue of High Performance Steel Connections of a Hybrid Girder Bridge in the Canadian Context." The research program will involve experimental tests on welded connections between high performance steel and

conventional steel to assess fatigue strength and the viability of hybrid high-performance steel girders.

The Jackson Fellowship will be presented to Leprince this year at the SSEF Annual Conference in St. John's, Newfoundland, on October 3.

Information about the Jackson Fellowship can be found on the SSEF website. (www.ssef-ffca.ca/scholarships/jackson).

#### 2013 SSEF University Research Grants

The SSEF has been actively promoting research of topics that are considered to be of interest and importance to the steel industry since 1995. University research grant applications are reviewed and ranked by the SSEF and, at the discretion of the SSEF, awarded to full-time members of engineering faculties of Canadian universities for a one-year period. The total value of grants awarded for the 2013-2014 academic year is \$102,000. The principal researcher of the topranked SSEF university research grant applications is also awarded the H. A. Krentz Award.

The 2013-2014 grant recipients and topics include: Dr. Robert Driver (University of Alberta), "Solving the mystery of double-coped beams"; Dr. Anjan Bhowmick (Concordia University), "Behaviour of light-gauge steel shear walls with screwed infill plate connections for regions of lowto-moderate seismicity"; Dr. Dimitrios Lignos (McGill University), "Development of Ry, Rt factors and probable brace resistance axial loads for the seismic design of bracing connections and other members"; Dr. Scott Walbridge and Dr. Jeffrey West (University of Waterloo), "Fatigue behaviour and design of shear connectors in steel-precast composite girders"; and Dr. Tony T.Y. Yang (University of British Columbia), "Development of innovative and cost-effective seismic fuses using wide flange steel sections."

Information about these research topics, as well as those from previous grant years, can be found on the SSEF website.

Suggestions for research topics can be made by completing the "SSEF Research Topic Suggestion Form" found on the SSEF website at www.ssef-ffca.ca/research.

#### 2013 H.A. Krentz Award

The H.A. Krentz Award recognizes a researcher whose research topic has special merit and interest with promise that it will make a significant contribution to understanding the behaviour of steel structures, advances in the economy, safety or reliability of steel structures. A gift of \$5,000 is part of this notable award.



Dr. Robert Driver (left) being presented with his award by SSEF Governor Chris Adach (right)

The 2013 H.A. Krentz Award is awarded to Dr. Robert Driver, Professor, Department of Civil and Environmental Engineering at the University of Alberta. The SSEF awarded Dr. Driver a grant of \$22,000 for his research on "Solving the mystery of double-coped beams."



Dr. Robert Driver Ph.D., P. Eng., has over 25 years of experience in the steel industry, applied research related to steel structures, structural consulting and engineering education. Dr. Driver's primary research interests pertain to the design and behaviour of steel structures, including topics such as bolted and welded connections, plate walls, high performance steel, rehabilitation, composite columns, and behaviour under extreme loading.

#### 2013 Architectural Student Design Competition

Since it was announced in 2001, the Architectural Student Design Competition has encouraged architectural students to consult with experts, engineers and fabricators to arrive at a true understanding of the structural design and detailing requirements of a steel structure – taking the study of steel beyond the technical and into the realm of supposed application to arrive at a meaningful realization of architectural ideas. Eligibility for this competition is limited to students registered in professional architectural programs in Canada.

Submissions for this competition are examined by a panel of judges that includes an architectural educator, a practicing architect, a consulting structural engineer and a structural steel fabricator. The top three submissions receive awards.

The 2013 competition challenged students to include the theme of "POP-UP" in their designs. Below is the description of "The Challenge," as given in the 2013 competition poster (see also www.ssef-ffca.ca/competitions/ssef/2013):

"In her article *Pop-Up Populism*, on the growing phenomenon of POP-UP architecture, Kelly Chan writes:

Vitruvius's virtues roughly translate to "utility," "durability," and "beauty." But for centuries now, this association of great architecture with fixed and timeless permanence, along with the entire Vitruvian triad, has been losing traction. Our environment has been built, altered, and rebuilt in overlapping waves. While some buildings stand the test of



Award of Excellence Winners: Gabriella den Elzen and James Clarke-Hicks



Award of Excellence: "Shape Space" panel by Gabriella den Elzen and James Clarke-Hicks, University of Waterloo

time, most seem to expire in relevance. Grand architectural and planning schemes are increasingly rare. In fact, we fast-forward to today, and it seems that we are collectively swinging towards a polar opposite of Vitruvian values. We are moving towards an architecture in which the permanent is becoming a lot less permanent.

www.artinfo.com/news/story/802841/pop-up-populismhow-the-temporary-architecture-craze-is-changing-ourrelationship-to-the-built-environment

A related movement articulated by New York's Projects for Public Spaces calls for a new set of Vitruvian principles: "Light, Quick and Cheap," as a response to contemporary cities struggling to do more with less, to find creative, innovative and quick ways of addressing urban issues, and to respond to their communities in a meaningful fashion. Projects such as Brooklyn's DeKalb Market, Oakland's Popuhood, San Francisco's parking stall parks, and a multitude of gallery and market installations are manifesting and testing these new principles. Temporary in more than the temporal sense, these designs eschew disposability in favour of changeability: they are responsive to change in use and time. Students are invited to engage in an exploration of POP-UP as an architectural and structural concept. To that end, we encourage students to conceptualize and design a POP-UP architectural installation that incorporates the goals of being: (truly) sustainable; temporary; socially relevant; responsive to site.

While they may range from utilitarian to exquisite in their execution, all responses must come to terms with one simple problem: the clear incorporation of POP-UP in a design that utilizes steel as the primary element for structural form."

Students were supposed to conceptualize, and realize in detail, a structure that explores the theme of "POP-UP" with emphasis on the architectural exploration through form and

material and on the essential relationship between architecture and structure. Students were required to include buildable details, primarily using structural steel, and were to collaborate with fabricators on those details.

#### Award winners

The awards were presented at the SSEF – CISC Annual Convention on September 20, 2013 in Whistler, B.C. The award-winning submissions are featured on the SSEF website (www.ssef-ffca.ca/competitions/ssef/2013).

#### Award of Excellence

Gabriella den Elzen and James Clarke-Hicks, University of Waterloo

Faculty Sponsors: Terri Meyer Boake & Mark Cichy

Gabriella and James were awarded \$3,000 (to share) and the Faculty Sponsors were awarded \$1,500 (to share).

#### Awards of Merit

Ji Shi and Logan Steele, University of Waterloo

Faculty Sponsors: Terri Meyer Boake & Mark Cichy

Ji and Logan were awarded \$2,000 (to share) and the Faculty Sponsors were awarded \$1,000 (to share).

Gary Luk, Ryerson University

Faculty Sponsor: Vincent Hui

Gary was awarded \$2,000 and the Faculty Sponsor was awarded \$1,000.

Please visit the SSEF website to view the submissions of the award winners and to also get information about the 2014 SSEF Architectural Design Competition, "Span" (www.ssef-ffca.ca/competitions/ssef).

#### Common Codes and Standards for Design and Construction of Steel Structures Current Status and Future Publication Targets

<b>Current Status and Future Publication Targe</b>	ts		
CODE/STANDARD/SUPPLEMENT/ COMMENTARY/REFERENCED DOCUMENT	CURRENT EDITION	NEXT EDITION/ REVISION	PUBLICATION TARGET
National Building Code of Canada (NBC)	NBC 2010	NBC 2015	Late 2015
NBC Structural Commentaries (Part 4 of Div. B)	NBC 2010 Str. Comm.	NBC 2015 Str. Comm.	2016
CSA S16 Design of Steel Structures	CSA \$16-14	ТВА	
CISC Commentary on CSA S16 (Part 2 of CISC Handbook of Steel Construction)	CISC Handbook 10th Edition <sup>1</sup>	CISC Handbook 11th Edition <sup>2</sup>	2015
CISC Moment Connections for Seismic Applications	2nd Edition	ТВА	
CSA S6 Canadian Highway Bridge Design Code	CSA \$6-06	S6-14	Fall 2014
- Supplements to CSA S6	CSA S6S3-13	None planned	
CSA S6.1 Commentary on Canadian Highway Bridge Design Code	CSA \$6.1-06	S6.1-14	Fall 2014
- Supplements to CSA S6.1	CSA S6.1S3-13	None planned	
CSA G40.20/G40.21 General Requirements for Rolled or Welded Structural Quality Steel/Structural Quality Steel	G40.20-13 G40.21-13	ТВА	
CSA W59 Welded Steel Construction (Metal Arc Welding)	CSA W59-13	ТВА	
CSA W47.1 Certification of Companies for Fusion Welding of Steel	CSA W47.1-09	W47.1-15	2015
CSA S136 North American Specification for the Design of Cold- Formed Steel Structural Members	CSA \$136-12	ТВА	
CSA \$136.1 Commentary on CSA \$136	CSA \$136.1-12	ТВА	

<sup>1</sup>CISC Handbook of Steel Construction - 10th Edition includes CSA S16-09, its Commentary, CISC Code of Standard Practice - 7th Edition, and design and detailing aids in accordance with CSA S16-09 <sup>2</sup>CISC Handbook of Steel Construction - 11th Edition includes CSA S16-14, its Commentary, CISC Code of Standard Practice - 7th Edition, and design and detailing aids in accordance with CSA S16-14

Member and Associate list as of	June 12, 2014	Canam,
Legend: *sales office only		St-Georges, QC www.canam.w
B Buildings Br Bridges S Structural P Platework		Charper Boucherville, G www.sofab.ca
J Open-web Steel Joist		Construe St. Nazaire, Qu www.proco.ca
STEEL FABRICATOR ATLANTIC		Lainco II Terrebonne, Q
Canam, a division of Canam Group In Moncton. NB	<b>nc.</b> 506-857-3164	<b>Les Acie</b> Charlesbourg,
www.canam-construction.com		Les Cons Atlas in
Cherubini Metal Works Limited	P, S	Ste-Marie de B
Dartmouth, NS www.cherubiniaroup.com	902-468-5630	Les Indu
Eascan Building Sy Truro, NS	vstems Ltd. S 902-897-9553	Longueuil, QC www.industrie
www.eascan.ca		Les Strue St-Romuald, Q
Gerrys Weiding & Fabrication Inc. St-John, NB	<b>B, S</b> 506-642-3704	www.structure
MacDougall Steel	Erectors Inc. 902-855-2100	Rimouski, QC www.structure
Marid Industries Li	imited S	Montmagny, C
Windsor Junction, NS www.marid.ns.ca	902-860-1138	Métal Pe Donnaconna, ( www.metalner
Modular Fabricatio Miramichi, NB www.modularfab.com	on Inc. S 506-622-1900	Mometa Varennes, QC
MQM Quality Manufacturing Ltd Tracadie-Sheila, NB www.mgm.ca	• <b>P, S</b> 506-395-7777	www.mometal NGA Str Drummondville www.nga.qc.cc
Ocean Steel &		Produits
Construction Ltd. Saint John, NB www.oceansteel.com	<b>Br, P, S</b> 506-632-2600	Rimouski, QC www.pmibuild
Prebilt Structures I Charlottetown, PE www.prebiltsteel.com	.td. P, S 902-892-8577	Beauceville, Qi www.quirionm
Ready Arc Welding (2000) Inc. Saint John, NB www.readvarc.ca	<b>9</b> <b>B, Br, P, S</b> 506-696-8336	Joliette, QC Structal- of Cana
RKO Steel Limited Dartmouth, NS	<b>P, S</b> 902-468-1322	www.structalp
Tek Steel Ltd. Fredericton, NB	<b>S</b> 506-452-1949	Construe of Cana
QUEBEC		www.structalst
Acier Fortin Inc. Montmagny, QC www.acierfortin.com	<b>S</b> 418-248-7904	Sturo Ma Lévis, QC www.sturomet
Acier Métaux Spec Chateauguay, QC www.metauxspec.ca	<b> inc. S</b> 450-698-2161	Superme St-Romuald, Q www.superme
Acier Profilé SBB In Terrbonne, QC www.sbb.ca	nc. <b>B, Br, J</b> 450-968-0800	Tecno M Quebec, QC www.tecnome
Acier Robel inc. St-Eustache, QC	<b>S</b> 450-623-8449	ONTARI A.J. Brg
<b>Alma Soudure inc.</b> Alma, QC	<b>S</b> 418-669-0330	Kitchener, ON www.ajbraun.o
www.almasoudure.com		AC Meta Oldcastle, ON
of Canam Group In Saint-Gédéon, QC	nc. J, S 418-582-3331	ACL Stee Kitchener, ON www.aclsteel.c

<b>Canam, a division of Canam Group Inc.</b> HGeorges, QC ww.canam.ws	<b>J, S</b> 418-228-8031
Charpentes d'acier Sofal oucherville, QC ww.sofab.ca	<b>b Inc. S</b> 450-641-2618
Constructions PROCO Inc t. Nazaire, QC ww.proco.ca	<b>. S</b> 418-668-3371
ainco Inc. errebonne, QC	<b>B, Br, S</b> 450-965-6010
harlesbourg, QC	418-841-7771
es Constructions Beauce Atlas inc. te-Marie de Beauce, QC ww.beauceatlas.ca	<b>Br, S</b> 418-387-4872
es Industries V.M. inc. ongueuil, QC ww.industriesvm.com	<b>S</b> 450-651-4901
es Structures C.D.L. Inc. Homuald, QC ww.structurescdl.com	<b>S</b> 418-839-1421
es Structures GB Ltée imouski, QC ww.structuresgb.com	<b>P, S</b> 418-724-9433
<b>Λétal Moro inc</b>	<b>S</b> 418-248-1018
Aétal Perreault Inc. onnaconna, QC www.metalperreault.com	<b>B, P, S</b> 418-285-4499
Aometal Structures Inc. arennes, QC	<b>B, S</b> 450-929-3999
<b>IGA Structure Inc.</b> rummondville, QC ww.nga.gc.ca	<b>B, S</b> 819-477-6891
Produits Métalliques PM imouski, QC ww.pmibuildina.com	418-723-2610
Quirion Métal Inc. eauceville, QC ww.guirionmetal.com	<b>S</b> 418-774-9881
<b>Ray Metal Joliette Ltée</b>	<b>S</b> 450-753-4228
structal-Bridges, a divisi	on
uébec, QC ww.structalponts.com	418-683-2561
structal-Heavy Steel construction, a division of Canam Group Inc. oucherville, QC	<b>J, S</b> 450-641-4000
Sturo Metal Inc.	<b>S</b> 418-833-2107
ww.suoiniena.com Supermétal Structures In Homuald, QC www.supermetal.com	<b>c. P, S</b> 418-834-1955
<b>iecno Metal Inc.</b> uebec, QC ww.tecnometal.ca	<b>B, S</b> 418-682-0315
ONTARIO	_
A.J. Braun Mfg. Limited itchener, ON ww.ajbraun.com	<b>Br</b> 519-745-5812
AC Metal Fabricating Ltd Idcastle, ON	519-737-6007
N <b>CL Steel Ltd.</b> itchener, ON ww.aclsteel.ca	<b>S</b> 519-568-8822

Arkbro Structures Mississauga, ON www.arkbrostructures.com	<b>S</b> 905-766-4038
Azimuth Three Enterprise Brampton, ON www.az3.com	es Inc. S 905-793-7793
Benson Steel Limited Bolton, ON www.hensonsteel.com	<b>J, S</b> 905-857-0684
Burnco Mfg. Inc. Concord, ON www.burncomfg.com	<b>S</b> 905-761-6155
C & A Steel (1983) Ltd. Sudbury, ON www.casteel1983.com	<b>S</b> 705-675-3205
C_ore Metal Inc. Oakville, ON www.coremetal.com	<b>S</b> 905-829-8588
Canam, a division of Canam Group Inc. (Ontario) Mississauga, ON www.canam-construction.com	<b>J, S</b> 905-671-3460
Central Welding & Iron Works Group North Bay, ON www.centralwelding.ca	<b>B, Br, P, S</b> 705-474-0350
Cooksville Steel Limited [Kitchener] Kitchener, ON www.cooksvillesteel.com	<b>S</b> 519-893-7646
Cooksville Steel Limited [Mississauga] Mississauga, ON www.cooksvillesteel.com	<b>S</b> 905-277-9538
D & M Steel Ltd. Newmarket, ON	<b>S</b> 905-836-6612
Eagle Bridge Inc. Kitchener, ON www.eaglebridge.ca	<b>Br, S</b> 519-743-4353
Ed Lau Ironworks Limite Kitchener, ON www.edlau.com	d S 519-745-5691
Fortran Steel Contracting Ottawa, ON www.fortransteel.com	<b>613-821-4014</b>
G & P Welding and Iron Works North Bay, ON www.gpwelding.com	<b>P, S</b> 705-472-5454
Gensteel - Division of Au Steel Group Inc.	ustin S
www.gensteel.ca	905-799-3324
Welland, ON www.supremearoup.com	905-732-6018
IBL Structural Steel Limit Mississauga, ON www.iblsteel.com	ed B 905-671-3301
Lambton Metal Services Sarnia, ON www.lambtonmetalservice.ca	<b>S</b> 519-344-3939
Laplante Welding of Cornwall Inc. Cornwall, ON	<b>S</b> 613-938-0575
www.laplantewelding.com Linesteel (1973) Limited Barrie, ON	<b>B, S</b> 705-721-6677
www.linesteel.com Lorvin Steel Ltd. Brampton, ON www.lorvinsteel.com	<b>S</b> 905-458-8850

M&G Steel Ltd. Oakville, ON	<b>S</b> 905-469-6442
www.mgsteel.ca M.I.G. Structural Steel ( 3526674 Canada Inc.)	(Div. of S
St-Isidore, ON www.miasteel.com	613-524-5537
Maple Industries Inc. Chatham, ON	<b>S</b> 519-352-0375
Mariani Metal Fabricat	ors
Limited Etobicoke, ON www.marianimetal.com	<b>S</b> 416-798-2969
Mirage Steel Limited Brampton, ON www.miragesteel.com	<b>J, S</b> 905-458-7022
Norak Steel Construction Limited Concord, ON www.noraksteel.com	<b>S</b> 905-669-1767
Paradise Steel Fab. Ltd Etobicoke, ON	• <b>S</b> 905-770-2121
Paramount Steel Limite Brampton, ON www.paramountsteel.com	ed S 905-791-1996
Pittsburgh Steel Group Mississauga, ON www.pittsburghsteel.com	<b>S</b> 905-362-5097
Quad Steel Inc. Bolton, ON www.quadsteel.ca	<b>S</b> 905-857-9404
Quest Steel Inc. Mississauga, ON	<b>B, Br, P, S</b> 905-564-7446
Refac Industrial Contractors Inc. Harrow, ON www.refacindustrial.com	<b>P, S</b> 519-738-3507
Refac Industrial Contractors Inc. Harrow, ON www.refacindustrial.com Sandro Steel Fabricatic Sudbury, ON	P, S 519-738-3507 on Ltd. 705-522-1305
Refac Industrial Contractors Inc. Harrow, ON www.refacindustrial.com Sandro Steel Fabricatic Sudbury, ON Shannon Steel Inc. Orangeville, ON www.shannonsteel.com	P, S 519-738-3507 on Ltd. 705-522-1305 S 519-941-7000
Refac Industrial Contractors Inc. Harow, ON www.refacindustrial.com Sandro Steel Fabricatic Sudbury, ON Shannon Steel Inc. Orangeville, ON www.shannonsteel.com Steelcon Fabrication In- Bolton, ON	P, S 519-738-3507 on Ltd. 705-522-1305 S 519-941-7000 c. B 416-798-3343
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Refac Industrial Contractors Inc. Harrow, ON www.refaindustrial.com Sandro Steel Fabricatic Sudbury, ON Shannon Steel Inc. Orangeville, ON www.shannonsteel.com Steelcon Fabrication In- Bolton, ON Telco Steel Works Ltd. Guelph, ON www.telcosteelworks.ca Tower Steel Company I Erin, ON www.towersteel.com Trade-Tech Industries, I Bowmanville, ON www.tradetch.ca	P, S 519-738-3507 on Ltd. 705-522-1305 S 519-941-7000 c. B 416-798-3343 S 519-837-1973 Ltd. S 519-833-7520 Inc. B, P, S 905-623-5060
Refac Industrial Contractors Inc. Harow, ON www.refacindustrial.com Sandro Steel Fabricatic Sudbury, ON Shannon Steel Inc. Orangeville, ON www.shannonsteel.com Steelcon Fabrication Inc Bolton, ON Telco Steel Works Ltd. Guelph, ON www.telcosteelworks.co Tower Steel Company I Erin, ON www.towersteel.com Trade-Tech Industries, I Bowmanville, ON www.tradetech.co	P, S 519-738-3507 705-522-1305 519-941-7000 c. B 416-798-3343 519-837-1973 Ltd. S 519-833-7520 Inc. B, P, S 905-623-5060 ses Ltd. S 905-795-8757
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Refac Industrial Contractors Inc. Harow, ON www.refacindustrial.com Sandro Steel Fabricatic Sudbury, ON Shannon Steel Inc. Orangeville, ON www.shannonsteel.com Steelcon Fabrication Inc Bolton, ON Telco Steel Works Ltd. Guelph, ON www.telcosteelworks.co Tower Steel Company I Erin, ON www.tadetech.co Trade-Tech Industries, I Bowmanville, ON www.tradetech.co Tresman Steel Industrie Mississouga, ON www.tradetech.com Victoria Steel Corporat Oldcastle, ON Walters Inc. Hamilton, ON www.udtetsinc.com	P, S 519-738-3507 705-522-1305 S 519-941-7000 c. B 416-798-3343 S 519-837-1973 Ltd. S 519-833-7520 Inc. B, P, S 905-623-5060 es Ltd. S 905-795-8757 ion S 519-737-6151 Br, P, S 905-388-7111
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**P, S** 807-623-4844

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Omega Joists Inc. Calgary, AB www.omegajoists.com	<b>J</b> 403-250-7871
Shopost Iron Works (198 Winnipeg, MB www.shopost.com	<b>B9) Ltd. S</b> 204-233-3783
Sperling Industries Ltd. Sperling, MB www.sperlingind.com	<b>B, Br, P, S</b> 204-626-3401
Supreme Steel LP [Winni Winnipeg, MB www.supremearoup.com	ipeg] B, S 204-589-7371
SASKATCHEWAN	
Anlin Welding & Steel	
Regina, SK	<b>B, S</b> 306-721-6566
www.anlinwelding.com	Colleds
Saskatoon, SK www.elancesteel.com	306-931-4412
IWL Steel Fabricators Ltc Saskatoon, SK www.iwlsteel.com	I. P, S 306-242-4077
Omega Joists Inc. Calgary, AB www.omegajoists.com	<b>J</b> 403-250-7871
Supreme Group Inc. [Saskatoon] Saskatoon, SK www.supremearoun.com	<b>P, S</b> 306-975-1177
Weldfab Ltd. Saskatoon, SK www.weldfab.com	<b>S</b> 306-955-4425
ALBERTA	
Anglia Steel Industries	R D C
Anglia Steel Industries (1984) Calgary, AB	<b>B, P, S</b> 403-720-2363
Anglia Steel Industries (1984) Calgary, AB www.angliasteel.ca Bow Ridge Steel Fabrica	<b>B, P, S</b> 403-720-2363 ting <b>S</b>
Anglia Steel Industries (1984) Calgary, AB www.angliasteel.ca Bow Ridge Steel Fabrica Calgary, AB	<b>B, P, S</b> 403-720-2363 <b>ting S</b> 403-230-3705
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Anglia Steel Industries (1984) Calgary, AB www.angliasteel.ca Bow Ridge Steel Fabrica Calgary, AB C.W. Carry (1967) Ltd. Edmonton, AB www.cwcarry.com Canam, a division of Canam Group Inc.	<b>B</b> , <b>P</b> , <b>S</b> 403-720-2363 <b>ting S</b> 403-230-3705 <b>P</b> , <b>S</b> 780-465-0381
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Anglia Steel Industries (1984) Calgary, AB www.cangliasteel.ca Bow Ridge Steel Fabrica Calgary, AB C.W. Carry (1967) Ltd. Edmonton, AB www.cwarry.com Canam, a division of Canam Group Inc. (Alberta) Calgary, AB www.conam-construction.com	<b>B</b> , <b>P</b> , <b>S</b> 403-720-2363 <b>ting S</b> 403-230-3705 <b>P</b> , <b>S</b> 780-465-0381 <b>J</b> , <b>S</b> 403-252-7591
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www.northern-weldarc.com	100 107 1522
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Precision Steel & Manufacturing Ltd. Edmonton, AB	<b>S</b> 780-449-4244
Rampart Steel Ltd. Edmonton, AB www.rampartsteel.com	<b>S</b> 780-465-9730
Rapid-Span Bridges Inc. County of Grande Prairie No. 1, AB	<b>Br</b> 780-538-9199
RIMK Industries Inc. Calgary, AB	<b>B, S</b> 403-236-8777
Spartan Steel Edmonton, AB	<b>S</b> 780-435-3807
Supermétal Structures In	ю.,
Leduc, AB www.supermetal.com	<b>P, 5</b> 780-980-4830
Supreme Steel Ltd. [Edmonton] Edmonton, AB www.supremearoup.com	<b>P, S</b> 780-483-3278
Supreme Steel LP, Bridge Division Edmonton, AB www.supremegroup.com	<b>P, S</b> 780-467-2266
Tarpon Energy Services (Structures) Ltd. Calgary, AB www.tarponenergy.com	<b>B, S</b> 403-236-9293
Triangle Steel (1999) Ltd Calgary, AB	• <b>P, S</b> 403-279-2622
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